

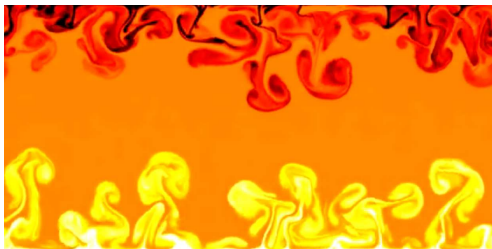
On models for viscoelastic fluid-like materials  
that are mechanically incompressible and  
thermally compressible or expansible and their  
Oberbeck–Boussinesq type approximations

Vít Průša (joint work with K.R. Rajagopal)  
`prusv@karlin.mff.cuni.cz`

Mathematical Institute, Charles University

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# Buoyancy driven flows



# Oberbeck–Boussinesq approximation

Original papers:

- ▶ J. Boussinesq. *Théorie analytique de la chaleur*. Gauthier-Villars, Paris, 1903
- ▶ A. Oberbeck. Über die Wärmeleitung der Flüssigkeiten bei Berücksichtigung der Strömungen infolge von Temperaturdifferenzen. *Ann. Phys. Chem.*, 1:271, 1879

# Oberbeck–Boussinesq approximation

Governing equations:

$$\operatorname{div} \mathbf{v} = 0$$

$$\rho_{\text{ref}} \frac{d\mathbf{v}}{dt} = -\nabla m + \mu_{\text{ref}} \Delta \mathbf{v} + \rho_{\text{ref}} (1 + \alpha(\theta - \theta_{\text{ref}})) \mathbf{b}$$

$$\rho_{\text{ref}} c_{m,\text{ref}} \frac{d\theta}{dt} = \kappa \Delta \theta$$

Rayleigh number:

$$\text{Ra} =_{\text{def}} \frac{\rho_{\text{ref}} g \alpha_{\text{ref}} \theta_{\text{diff}} l_{\text{char}}^3}{k \eta_{1,\text{ref}}}$$

# Full system of governing equations

Governing equations:

$$\frac{d\rho}{dt} + \rho \operatorname{div} \mathbf{v} = 0$$

$$\rho \frac{d\mathbf{v}}{dt} = \operatorname{div} \mathbb{T} + \rho \mathbf{b}$$

$$\rho \frac{de}{dt} = \mathbb{T} : \mathbb{D} - \operatorname{div} \mathbf{q}$$

Constitutive relations:

$$\mathbb{T} = -p\mathbb{I} + 2\mu\mathbb{D}$$

$$\mathbf{q} = -\kappa\nabla\theta$$

$$p = p(\rho, \theta)$$

$$e = e(\dots)$$

## Oberbeck–Boussinesq approximation

- ▶ E. A. Spiegel and G. Veronis. On the Boussinesq approximation for a compressible fluid. *Astrophys. J.*, 131:442–447, 1960

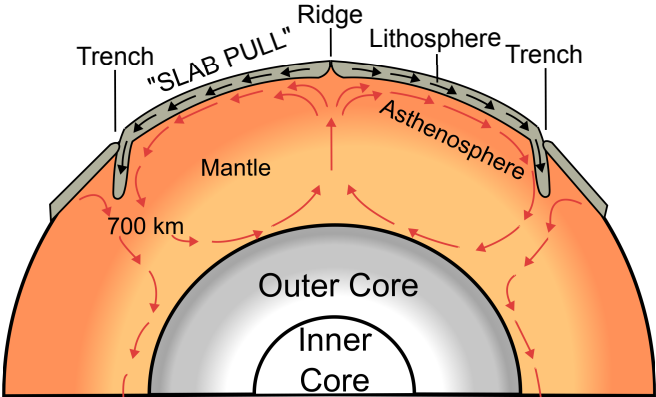
*In equation (19) we have retained the term  $g\varepsilon(\rho'/\Delta\rho_0)\mathbf{k}$  even though it contains  $\varepsilon$  as a factor.*

- ▶ John M. Mihaljan. A rigorous exposition of the Boussinesq approximations applicable to a thin layer of fluid. *Astrophys. J.*, 136:1126–1133, 1962
- ▶ K. R. Rajagopal, M. Růžička, and A. R. Srinivasa. On the Oberbeck–Boussinesq approximation. *Math. Models Methods Appl. Sci.*, 6(8):1157–1167, 1996

# Oberbeck–Boussinesq system as an approximation of an “exact” system

- ▶ Mechanically and thermally compressible/expansible material ( $\text{Ma} \approx \varepsilon$ ,  $\text{Fr} \approx \sqrt{\varepsilon}$ ).  
Eduard Feireisl and Antonin Novotný. The Oberbeck–Boussinesq approximation as a singular limit of the full Navier–Stokes–Fourier system. *J. Math. Fluid Mech.*, 11:274–302, 2009
- ▶ Mechanically incompressible and thermally compressible/expansible material.  
K. R. Rajagopal, M. Růžička, and A. R. Srinivasa. On the Oberbeck–Boussinesq approximation. *Math. Models Methods Appl. Sci.*, 6(8):1157–1167, 1996

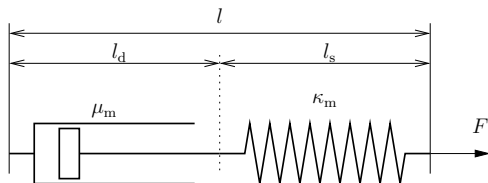
# Buoyancy driven flows in viscoelastic fluids



Source: Wikipedia



# Viscoelastic fluids – Maxwell model



Mechanical analogue:

- ▶ Spring – energy storage.
- ▶ Dashpot – energy dissipation.

Problems:

- ▶ Distribution of the deformation between the elements (spring, dashpot).
- ▶ Three dimensional model. (*Galilean invariance.*)
- ▶ Meets laws of thermodynamics. (*No perpetual motion.*)

## Upper convected Maxwell model

A three-dimensional incompressible viscoelastic rate type model:

$$\begin{aligned}\mathbb{T} &= -p\mathbb{I} + \mathbb{S} \\ \tau \overset{\nabla}{\mathbb{S}} + \mathbb{S} &= 2\mu\mathbb{D} \\ \operatorname{div} \mathbf{v} &= 0\end{aligned}$$

$$\begin{aligned}\mathbb{D} &=_{\text{def}} \frac{1}{2} \left( \nabla \mathbf{v} + (\nabla \mathbf{v})^T \right) \\ \mathbb{L} &=_{\text{def}} \nabla \mathbf{v} \\ \overset{\nabla}{\mathbb{A}} &=_{\text{def}} \frac{d\mathbb{A}}{dt} - \mathbb{L}\mathbb{A} - \mathbb{A}\mathbb{L}^T\end{aligned}$$

# Oberbeck–Boussinesq approximation for viscoelastic fluids

Governing equations:

$$\operatorname{div} \mathbf{v} = 0$$

$$\rho_{\text{ref}} \frac{d\mathbf{v}}{dt} = \operatorname{div} \mathbb{T} + \rho_{\text{ref}} (\mathbf{1} + \alpha(\theta - \theta_{\text{ref}})) \mathbf{b}$$

$$\rho_{\text{ref}} c_{m,\text{ref}} \frac{d\theta}{dt} = \kappa \Delta \theta$$

**Naive** approach is to replace Navier–Stokes fluid model

$$\mathbb{T} = -p\mathbb{1} + 2\mu\mathbb{D}$$

by Maxwell model

$$\mathbb{T} = -p\mathbb{1} + \mathbb{S}$$

$$\tau \overset{\nabla}{\mathbb{S}} + \mathbb{S} = 2\mu\mathbb{D}$$

$$\operatorname{div} \mathbf{v} = 0$$

# Full model

## Requirements:

- ▶ Mechanically incompressible but thermally compressible/expansible materials. (Liquids.)
- ▶ Different nature of the pressure. (No equation of state. Liquids.)
- ▶ Viscoelastic fluid like materials. (Internal energy has a non-thermal contribution.)
- ▶ Interplay between all the effects.

## Simplification:

- ▶ Let us consider only constant material coefficients. (Temperature independent viscosity.)

# Plan

## Viscoelasticity:

- ▶ K. R. Rajagopal and A. R. Srinivasa. A thermodynamic framework for rate type fluid models. *J. Non-Newton. Fluid Mech.*, 88(3):207–227, 2000

## Mechanical incompressibility and thermal expansivity/compressibility:

- ▶ K. R. Rajagopal, M. Růžička, and A. R. Srinivasa. On the Oberbeck–Boussinesq approximation. *Math. Models Methods Appl. Sci.*, 6(8):1157–1167, 1996

## Example – viscous fluids

Internal energy *ansatz*:

$$e(\rho, \eta) = g(\rho)\eta + h(\rho)$$

Time derivative:

$$\frac{de}{dt} = \frac{\partial g}{\partial \rho} \frac{d\rho}{dt} \eta + g \frac{d\eta}{dt} + \frac{\partial h}{\partial \rho} \frac{d\rho}{dt}$$

Entropy production:

$$\rho \frac{d\eta}{dt} + \operatorname{div} \frac{\mathbf{q}}{\theta} = \frac{1}{\theta} \left( -\mathbf{q} \cdot \nabla \theta + \mathbb{T}_\delta : \mathbb{D}_\delta + \left( \alpha \rho^2 \frac{\partial h}{\partial \rho} - \rho \eta - \alpha m \right) \frac{d\theta}{dt} \right)$$

Second law satisfied if:

$$\mathbf{q} =_{\text{def}} -\kappa \nabla \theta, \quad \mathbb{T}_\delta =_{\text{def}} 2\mu \mathbb{D}_\delta \quad \alpha \rho^2 \frac{\partial h}{\partial \rho} - \rho \eta - \alpha m =_{\text{def}} 0$$

## Viscous fluids – result

$$\Gamma_1 \frac{d\vartheta^*}{dt^*} = \operatorname{div}^* \mathbf{v}^*$$

$$\rho^* \frac{d\mathbf{v}^*}{dt^*} = \Gamma_2 \left( \Delta^* \mathbf{v}^* + \frac{1}{3} \nabla^* (\operatorname{div}^* \mathbf{v}^*) \right) + \frac{1}{\Gamma_1} (-\nabla^* m^* + \rho^* \mathbf{b}^*)$$

$$\Gamma_4 \Gamma_2 \rho^* c_m^* \frac{d\vartheta^*}{dt^*} = \Gamma_3 \Gamma_2 \Delta^* \vartheta^* + 2\Gamma_2 \mathbb{D}_\delta : \mathbb{D}_\delta + \left( \vartheta^* + \frac{\theta_{\text{ref}}}{\theta_{\text{diff}}} \right) \frac{dm^*}{dt^*}$$

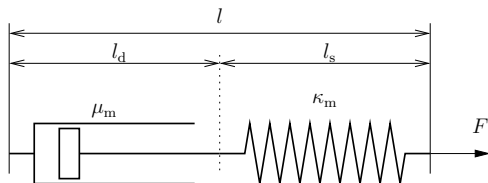
## Parameter values

	Experiment				
	Water	Water	Water	Glycerol	Mercury
$\Gamma_1$	$2.40 \times 10^{-5}$	$7.64 \times 10^{-4}$	$1.55 \times 10^{-2}$	$1.68 \times 10^{-2}$	$1.82 \times 10^{-3}$
$\Gamma_2$	$2.17 \times 10^{-1}$	$3.84 \times 10^{-2}$	$1.39 \times 10^{-5}$	$7.48 \times 10^{-3}$	$2.70 \times 10^{-5}$
$\Gamma_3$	$6.68 \times 10^7$	$6.68 \times 10^7$	$1.01 \times 10^6$	$1.15 \times 10^3$	$3.16 \times 10^7$
$\Gamma_4$	$2.19 \times 10^9$	$1.23 \times 10^{10}$	$3.18 \times 10^{11}$	$3.91 \times 10^8$	$2.89 \times 10^{10}$
Ra	$1.5 \times 10^2$	$4.8 \times 10^3$	$2.3 \times 10^{10}$	$4.5 \times 10^7$	$3.4 \times 10^7$
Pr	7.1	7.1	4.4	$2.5 \times 10^3$	$2.5 \times 10^{-2}$
Re	4.6	$2.6 \times 10^1$	$7.2 \times 10^4$	$1.3 \times 10^2$	$3.7 \times 10^4$

Table: Dimensionless parameters in some experiments with viscous fluids.



# Viscoelastic fluids – Maxwell model



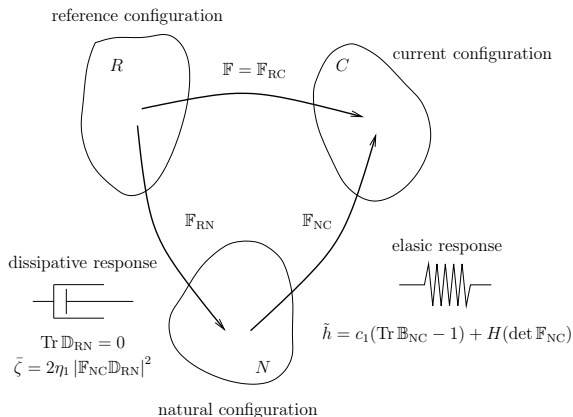
Mechanical analogue:

- ▶ Spring – energy storage.
- ▶ Dashpot – energy dissipation.

Problems:

- ▶ Distribution of the deformation between the elements (spring, dashpot).
- ▶ Three dimensional model. (*Galilean invariance.*)
- ▶ Meets laws of thermodynamics. (*No perpetual motion.*)

# Notion of natural configuration



Problem:

- Distribution of the deformation between the dissipative and elastic response. (Condition  $\mathbb{F} = \mathbb{F}_{NC} \mathbb{F}_{RN}$  is not enough restrictive.)

# Evolution equation for the elastic response

Evolution of the elastic response:

$$\frac{dB_{NC}}{dt} = \mathbb{L}B_{NC} + B_{NC}\mathbb{L}^T - 2F_{NC}D_{RN}F_{NC}^T$$

Oldroyd upper convected derivative:

$$\overset{\nabla}{A} =_{\text{def}} \frac{dA}{dt} - \mathbb{L}A - A\mathbb{L}^T.$$

Evolution equation for the elastic response:

$$\overset{\nabla}{B}_{NC} = -2F_{NC}D_{RN}F_{NC}^T$$

# Evolution equation for the internal energy

Internal energy *ansatz*:

$$e = g(\rho)\eta + \bar{h}(\tilde{l}_1(\mathbb{B}_{\text{NC}}), \tilde{l}_2(\mathbb{B}_{\text{NC}}), \det \mathbb{F}_{\text{NC}})$$

Evolution equation for the internal energy:

$$\frac{de}{dt} = \frac{\partial g}{\partial \rho} \frac{d\rho}{dt} \eta + g \frac{d\eta}{dt} + \frac{\partial \bar{h}}{\partial \tilde{l}_1} \frac{d\tilde{l}_1}{dt} + \frac{\partial \bar{h}}{\partial \tilde{l}_2} \frac{d\tilde{l}_2}{dt} + \frac{\partial \bar{h}}{\partial \det \mathbb{F}_{\text{NC}}} \frac{d}{dt} (\det \mathbb{F}_{\text{NC}})$$

Useful identities:

$$\frac{d}{dt} (\det \mathbb{F}_{\text{NC}}) = \det \mathbb{F}_{\text{NC}} (\text{Tr } \mathbb{D} - \text{Tr } \mathbb{D}_{\text{RN}})$$

$$\frac{\partial \bar{h}}{\partial \tilde{l}_1} \text{Tr} \frac{d\mathbb{B}_{\text{NC}}}{dt} = 2 \frac{\partial \bar{h}}{\partial \tilde{l}_1} \left( \mathbb{B}_{\text{NC}} : \mathbb{D} - \text{Tr} \left( \mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}} \mathbb{F}_{\text{NC}}^{\text{T}} \right) \right)$$

# Evolution equation for the entropy

Evolution equation for the entropy:

$$\begin{aligned} \rho\theta \frac{d\eta}{dt} = & -\operatorname{div} \mathbf{q} + \left( \mathbb{T}_\delta - 2\rho \frac{\partial \bar{h}}{\partial \tilde{\mathbf{l}}_1} (\mathbb{B}_{\text{NC}})_\delta \right) : \mathbb{D}_\delta \\ & + 2\rho \frac{\partial \bar{h}}{\partial \tilde{\mathbf{l}}_1} \operatorname{Tr} \left( \mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}} \mathbb{F}_{\text{NC}}^\top \right) \\ & + \left( -\alpha\rho \frac{\partial \bar{h}}{\partial \det \mathbb{F}_{\text{NC}}} \det \mathbb{F}_{\text{NC}} - \rho\eta - \alpha m - \frac{2}{3}\rho\alpha \frac{\partial \bar{h}}{\partial \tilde{\mathbf{l}}_1} \operatorname{Tr} \mathbb{B}_{\text{NC}} \right) \frac{d\theta}{dt} \\ & + \rho \frac{\partial \bar{h}}{\partial \det \mathbb{F}_{\text{NC}}} (\det \mathbb{F}_{\text{NC}}) \operatorname{Tr} \mathbb{D}_{\text{RN}} \end{aligned}$$

## Refinement of constitutive assumptions

“Solid” part is a compressible neo-Hookean elastic solid:

$$\tilde{h}(\tilde{I}_1, \tilde{I}_2, \det \mathbb{F}_{\text{NC}}) =_{\text{def}} c_1 (\tilde{I}_1 - 3) + H(\det \mathbb{F}_{\text{NC}})$$

“Fluid” part is incompressible:

$$\text{Tr } \mathbb{D}_{\text{RN}} =_{\text{def}} 0$$

Fourier's law:

$$\mathbf{q} =_{\text{def}} -\kappa \nabla \theta$$

Cauchy stress tensor:

$$\mathbb{T}_\delta =_{\text{def}} 2\rho \frac{\partial \tilde{h}}{\partial \tilde{I}_1} (\mathbb{B}_{\text{NC}})_\delta$$

Entropy:

$$\alpha \rho^2 \frac{\partial \tilde{h}}{\partial \rho} - \rho \eta - \alpha m - \frac{2}{3} \rho \alpha \frac{\partial \tilde{h}}{\partial \tilde{I}_1} \text{Tr } \mathbb{B}_{\text{NC}} =_{\text{def}} 0$$

# Entropy production

Entropy production:

$$\varsigma = 2\rho \frac{\partial \tilde{h}}{\partial \tilde{l}_1} \text{Tr} \left( \mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}} \mathbb{F}_{\text{NC}}^\top \right) + \kappa \frac{|\nabla \theta|^2}{\theta}$$

# Entropy production

Entropy production:

$$\varsigma = 2\rho \frac{\partial \tilde{h}}{\partial \tilde{I}_1} \text{Tr} \left( \mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}} \mathbb{F}_{\text{NC}}^{\top} \right) + \kappa \frac{|\nabla \theta|^2}{\theta}$$

Constitutive assumption:

$$\bar{\varsigma} =_{\text{def}} 2\eta_1 |\mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}}|^2$$

Maximization procedure leads to:

$$\mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}} \mathbb{F}_{\text{NC}}^{\top} = \frac{\rho}{\eta_1} \frac{\partial \tilde{h}}{\partial \tilde{I}_1} (\mathbb{B}_{\text{NC}} - \bar{\lambda} \mathbb{I})$$

Recall:

$$\overset{\vee}{\mathbb{B}}_{\text{NC}} = -2\mathbb{F}_{\text{NC}} \mathbb{D}_{\text{RN}} \mathbb{F}_{\text{NC}}^{\top}$$



# Generalized Maxwell model

Introduce notation:

$$\bar{\mathbb{S}} =_{\text{def}} \rho\mu_1 (\mathbb{B}_{\text{NC}} - \bar{\lambda}\mathbb{I}) \quad p =_{\text{def}} m + \rho\mu_1 \left( \frac{1}{3} \text{Tr} \mathbb{B}_{\text{NC}} - \bar{\lambda} \right)$$

Generalized Maxwell model:

$$\begin{aligned} \mathbb{T} &= -p\mathbb{I} + \bar{\mathbb{S}} \\ \frac{\eta_1}{\rho\mu_1} \overset{\nabla}{\bar{\mathbb{S}}} + \left( 1 + \frac{\eta_1}{\rho\mu_1} \text{div} \mathbf{v} \right) \bar{\mathbb{S}} &= 2\eta_1 \bar{\lambda} \mathbb{D}_\delta + \frac{2}{3} \eta_1 \bar{\lambda} (\text{div} \mathbf{v}) \mathbb{I} - \eta_1 \frac{d\bar{\lambda}}{dt} \mathbb{I} \end{aligned}$$

## Viscoelastic fluids – result

$$\Lambda_1 \frac{d\vartheta^*}{dt^*} = \operatorname{div}^* \mathbf{v}^*$$

$$\frac{1}{\operatorname{Pr}} \frac{\operatorname{Ra}^{\frac{2}{3}}}{\operatorname{Ra}_{\text{crit}}^{\frac{1}{6}}} \rho^* \frac{d\mathbf{v}^*}{dt^*} = \operatorname{div}^* \overline{\mathbf{S}}^*_{\delta} + \frac{\operatorname{Ra}^{\frac{1}{3}} \operatorname{Ra}_{\text{crit}}^{\frac{1}{6}}}{\Lambda_1} (-\nabla^* m^* + \rho^* \mathbf{b}^*)$$

$$\Lambda_2 \overline{\mathbf{S}}^*_{\delta} + (\rho^* + \Lambda_2 \operatorname{div}^* \mathbf{v}^*) \overline{\mathbf{S}}^* = 2\rho^* \bar{\lambda} \left( \mathbb{D}^*_{\delta} + \frac{1}{3} (\operatorname{div} \mathbf{v}) \mathbb{I} \right) - \rho^* \frac{d\bar{\lambda}}{dt^*} \mathbb{I}$$

$$\rho^* \frac{\operatorname{Ra}^{\frac{2}{3}}}{\operatorname{Ra}_{\text{crit}}^{\frac{1}{6}}} \frac{d\vartheta^*}{dt^*} = \Delta^* \vartheta^* + \frac{\Lambda_3 \rho^*}{\Lambda_2 2} \operatorname{Tr} \overline{\mathbf{S}}^*$$

$$+ \frac{2}{3} \Lambda_3 \Lambda_1 \left( \vartheta^* + \frac{\theta_{\text{ref}}}{\theta_{\text{diff}}} \right) \left[ \mathbb{D}^* : \overline{\mathbf{S}}^* + \frac{\rho^*}{\Lambda_2} \left( \bar{\lambda} \operatorname{div}^* \mathbf{v}^* - \frac{1}{2} \operatorname{Tr} \overline{\mathbf{S}}^* \right) \right]$$

$$+ \Lambda_3 \operatorname{Ra}^{\frac{1}{3}} \operatorname{Ra}_{\text{crit}}^{\frac{1}{6}} \left( \vartheta^* + \frac{\theta_{\text{ref}}}{\theta_{\text{diff}}} \right) \frac{dm^*}{dt^*}$$

# Parameter values

Parameter	Definition	Value
Pr	$\frac{\eta_{1,\text{ref}}}{\rho_{\text{ref}} k_{\text{ref}}}$	$4.0 \times 10^{23}$
Ra	$\frac{\rho_{\text{ref}} g \alpha_{\text{ref}} \theta_{\text{diff}} l_{\text{char}}^3}{k_{\text{ref}} \eta_{1,\text{ref}}}$	$5.6 \times 10^4$
$\Lambda_1$	$\alpha_{\text{ref}} \theta_{\text{diff}}$	$1.4 \times 10^{-2}$
$\Lambda_2$	$\frac{\tau_{\text{ref}}}{t_{\text{char}}}$	$1.5 \times 10^{-4}$
$\Lambda_3$	$\frac{\eta_{1,\text{ref}} l_{\text{char}}^2}{\kappa_{\text{ref}} \theta_{\text{diff}} t_{\text{char}}^2}$	$5.1 \times 10^{-1}$

**Table:** Dimensionless parameters for convection in the Earth's mantle.

# Conclusion

- ▶ Thermodynamically consistent model for mechanically incompressible Maxwell type fluids that are thermally compressible or expansible.
- ▶ Identification of the full system of the governing equations. (No Oberbeck–Boussinesq type approximation.)
- ▶ Discussion of the validity of the Oberbeck–Boussinesq type approximation in experiments/real problems involving viscoelastic fluids.

V. Průša and K. R. Rajagopal. On models for viscoelastic materials that are mechanically incompressible and thermally compressible or expansible and their Oberbeck–Boussinesq type approximations. *Math. Models Meth. Appl. Sci.*, 23(10):1761–1794, 2013